

# Supercritical CO<sub>2</sub> Extraction and Processing of Oilseeds

By

G.R. LIST, J.P. FRIEDRICH and J.W. KING

U.S. Department of Agriculture, Agricultural Research Service  
Northern Regional Research Center, Peoria, Illinois

## ABSTRACT

**S**UPERCritical CO<sub>2</sub> (SC-CO<sub>2</sub>) extraction of oilseeds is a viable alternative to expeller and/or hexane extraction methods. Petroleum solvents lack the desired solute specificity and often require extensive downstream refining to produce quality oil and meal. At 50° C and 8,000 psi, triglycerides are only partially soluble in SC-CO<sub>2</sub>, while at 80° and 12,000 they are completely miscible. A semicontinuous CO<sub>2</sub> extraction system is described that employs recycling SC-CO<sub>2</sub> at 3,000 psi to allow for flexibility in extraction of several vessels, either in series or parallel.

Characterization of crude soybean, corn, and cottonseed oils extracted under these conditions, show no increase in free fatty acids, phospholipids, or color at these higher extraction temperatures and flavor quality is maintained. By increasing SC-CO<sub>2</sub> extraction conditions (1600 gm flakes, 0.5-0.75 lbs CO<sub>2</sub>/min) from 50° C and 8,000 psi to 80° C and 12,000 psi, extraction times are reduced from several hours to as little as ten minutes. SC-CO<sub>2</sub> extraction of cottonseed at 80° C and 12,000 psi yields crude oil having 1.2 per cent weight free fatty acids and a Lovibond red of 20 (5-1/4" depth). SC-CO<sub>2</sub> extracted cottonseed oil shows no tendency to undergo color fixation while in storage.

Because of their low gum contents, SC-CO<sub>2</sub> extracted soy and corn oils can be steam refined to yield a bland flavor-stable edible oil. Although SC-CO<sub>2</sub> extracted cottonseed is too dark for steam refining, the crude cottonseed oil can be refined with 0.1 per cent excess of ten per cent caustic to yield 98 per cent neutral oil.

## INTRODUCTION

There has been a great deal of interest in supercritical fluid technology in the past ten years as evidenced by the scientific literature and popular articles in numerous news journals. One of the more active areas involves the extraction of oilseeds (1-16) with supercritical carbon dioxide (SC-CO<sub>2</sub>). Because CO<sub>2</sub> is presently used in food products such as carbonated beverages, it is generally regarded as a safe solvent (GRAS) for extraction of a variety of agricultural products, including oilseeds. Additional advantages of SC-CO<sub>2</sub> include its low cost, lack of flammability, and ease of separation from extracted products by phase separation.

## EXPERIMENTAL

### Process Considerations

The most extraordinary property SC-CO<sub>2</sub> exhibits is its ability to dissolve seed oils in all proportions at temperatures above 80° C and pressures of 12,000 psi (figure 1). During the supercritical extraction of the seed oil, the measured solubilities will take on finite values which are considerably less than the potential solubility of the oil in the dense gas phase. This is because the recorded solubilities are a function of the ratio of available oil in the seed to the SC-CO<sub>2</sub> present

in the extraction vessel.

For example, if the extraction vessel contained 100 g of soy flakes (20 per cent weight oil) and 100 g of SC-CO<sub>2</sub>, the maximum measured solubility would be 20 per cent, not the theoretically possible 100 per cent, as predicted by the phase diagram.

To illustrate this phenomena, an experiment was conducted in which six one-inch O.D. x 22 inch-high pressure tubes were filled with soybean flakes and placed in series with respect to the flowpath of the SC-CO<sub>2</sub>. Extraction was commenced at 12,000 psi and 90° C and under these conditions the initial flux of the oil into the SC-CO<sub>2</sub> produced a maximum solubility (wt. oil/wt. oil + wt. CO<sub>2</sub> passed) of 20.5 per cent. Upon reaching a quasi-steady state, the extraction experiment yielded an average solubility of 13.6 per cent, an amount still below the theoretical maximum oil solubility in SC-CO<sub>2</sub>.

This level of recorded solubility remained fairly constant throughout the extraction run until tubes five and six began to be depleted of oil. Residual oil and moisture content of the extraction tubes are reported in Table I. Note that the oil content of the residual meal ranged from a value of 0.91 per cent in tube one to 17.98 per cent in tube six.

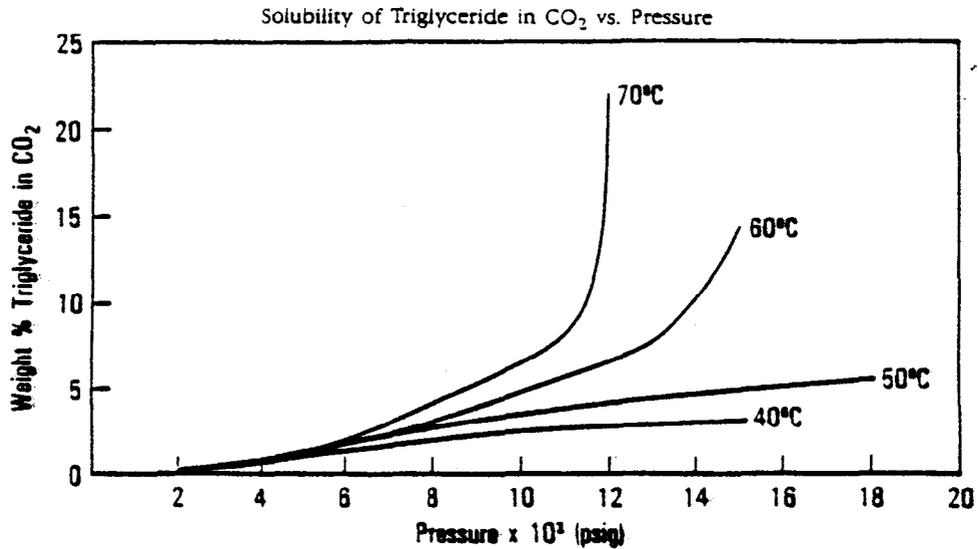
A similar experiment was also conducted using N<sub>2</sub> initially at a pressure of 12,000 psi and 90° C. Under these conditions, soybean oil is only sparingly soluble in the gas phase; hence the amount of oil vented from tube six in the nitrogen stream was negligible. However, when the N<sub>2</sub> flow was terminated, and CO<sub>2</sub> flow commenced into the extractor tubes, the oil flux into the supercritical fluid phase was initially enhanced to a maximum level of 43 weight per cent, due to the CO<sub>2</sub> contacting fresh oil as it moved through the seed bed.

These results document the appreciable solvent power of SC-CO<sub>2</sub> and the importance of the ratio of extractant to solvent (gas) in the extractor vessel. Residual oil and moisture analysis on the six extraction tubes utilized in the latter experiment are given in Table I.

Referring again to Figure 1, it is obvious that at temperatures below 55° C the solubility of triglycerides in SC-CO<sub>2</sub> is limited and shows a decreasing rate of increase at higher pressures. However, above 60° C the solubility increases rapidly with pressure, and at 70° C and 830 bar the verticality of the solubility curve indicates total miscibility. At 80° C and about 760 bar, the same trend is recorded.

Data from experiments conducted in a stirred autoclave further substantiate the solubility data (15). By the time the ideal pressure (760 bar) and temperature (80° C) are reached in the extraction vessel, the triglyceride is, for the most part, already extracted from the flaked seed and has been transferred to the SC-CO<sub>2</sub> phase. This can be essentially removed with one exchange of fresh SC-CO<sub>2</sub>, assuming essentially plug-flow with minimal mixing.

**FIGURE 1: SOLUBILITY OF TRIGLYCERIDES IN SC-CO<sub>2</sub> AS A FUNCTION OF TEMPERATURE AND PRESSURE**



**TABLE 1: EXTRACTION OF SOYBEAN FLAKES WITH SC-CO<sub>2</sub>\***

Time	CO <sub>2</sub>		N <sub>2</sub> /CO <sub>2</sub>	
	Mixture, %	Residual Oil, %	Mixture, %	Residual Oil, %
1	6.1	0.92	2.5	0.57
2	9.9	1.22	10.5	0.39
3	9.8	1.23	10.6	0.31
4	9.0	2.69	10.7	0.44
5	8.3	16.71	10.6	2.37
6	8.4	17.98	5.6	12.52

\*12,000 psi—80°C

**Equipment Considerations**

Because of the high solubility of seed oils in SC-CO<sub>2</sub>, it is possible to extract crushed and flaked or ground seed very rapidly by passing a stream of SC-CO<sub>2</sub> through the seed matrix at optimum extraction conditions (12,000 psi, 80° C) (8). Lowering the pressure as the oil-CO<sub>2</sub> solution leaves the extractor allows the oil to condense in a suitable receiver, and the CO<sub>2</sub> may be vented, stored, or recycled. A four-liter vessel filled with soy flakes (1600 gm) can be extracted by this method to a residual oil content of 0.5 per cent in eight minutes at a CO<sub>2</sub> flow rate of 125 to 190 l/min. Energy costs for compression and heat required for extraction are effectively offset by total recycle of the CO<sub>2</sub> at isothermal conditions. Recovery of oil is achieved by maintaining a pressure of 3,000 psi and a temperature of 80° C in the receiver. The oil-lean gas (0.03 per cent oil) is recompressed to extraction conditions and is recycled to the extraction vessel. The increased pressure assures that the oil remains in the dense-gas phase. Most of the energy of compression is

expended between 1,000 psi (supply-tank pressure) and 3,000 psi. Above this pressure, the relatively dense CO<sub>2</sub> behaves much like a liquid, and the costs of further compression to 12,000 psi are minimized. Likewise, the Joule-Thompson effect (cooling effect) caused by decompression of the CO<sub>2</sub> from 12,000 psi to 3,000 psi in the receiver is also minimized, because it is not allowed to expand at pressures below 3,000 psi where, once again, the cost of compression would be considerable.

The pressure drop is achieved by a variable back-pressure relief valve. The solute precipitates and is collected in the receiver. The low-pressure CO<sub>2</sub> is recycled through a mass-flowmeter to the compressor and back through the seed bed. The extraction is judged complete when no more solute is collected in the receiver. Based on the weight of CO<sub>2</sub> that has passed through the mass-flowmeter, the extraction can be easily duplicated.

The above concepts have resulted in construction of a

versatile extraction system (figure 2) that can be adopted to a variety of extraction configurations. For example, with proper valve sequencing, it is possible to flow in parallel or series, in either direction, through the multiple extraction vessels. The three-vessel system allows two vessels to be in the extraction mode while the third is being emptied and refilled.

The flow direction may also be reversed "momentarily" to prevent packing of the seed bed. A second smaller auxiliary gas supply and compressor has been integrated into the system (figure 2), to replace the small amount of CO<sub>2</sub> lost from the closed system due to the sampling of the extract or system leakage. A pressure gauge equipped with a electric-contact face, is used to interrupt power to the compressor and activate an alarm at a preset pressure safety below the rated system pressure.

The high-pressure extraction side of the system consists of all components downstream from the main compressor, up to and including the back-pressure relief valve (BPRV). The minimum pressure rating of these components is 20,000 psi. The four-liter A-286 rust resistant, steel alloy extraction vessels are rated at 30,000 psi and are fitted with self-energizing metal seal-ring head closures. The vessels are also fitted with rupture disc assemblies set at 15,000 psi. The 1/4 inch-high pressure valves and tubing used in the assembly are rated at 60,000 psi. The low-pressure side of the system includes the receiver

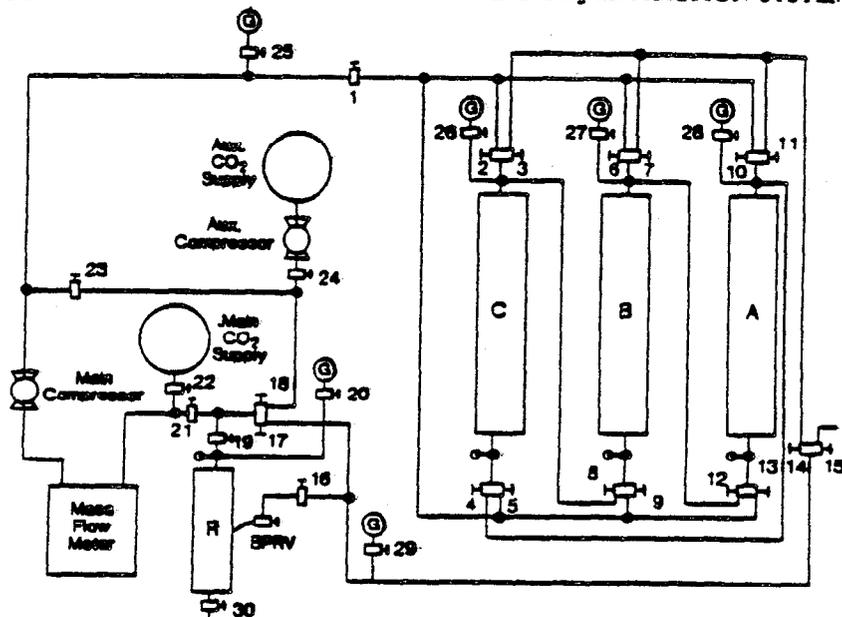
(10,000 psi), the mass flow meter (5,000 psi), and 1/4 inch low-pressure valves and tubing (10,000 psi) having larger bore to accommodate flow rates approaching two lb of CO<sub>2</sub>/min at 2,500 to 3,000 psi.

#### Seed Preparation and Extraction Procedure

Oilseeds, in this case soybeans, are cracked and dehulled, after which they are passed through flaking rolls to yield flakes with a thickness of about 0.01 inch. As flake thickness increases, oil yield decreases because of the inaccessibility of the oil to the CO<sub>2</sub> (16). Conversely, depending upon the fineness of the particles and their oil content, blockage of flow can result at very high solvent rates (16).

Heated Vessels A, B + C (figure 2) are filled with flaked seed after placing a filter underneath and on top of the seed bed to prevent particulates from being transported throughout the system. The vessels are sealed and, with the vent valves 15 and 30 closed, the entire system is allowed to fill with CO<sub>2</sub> through the mass-flowmeter to tank pressure of 900 psi. Vessel C is isolated and vessels A and B are pressurized to 12,000 psi. After extraction temperature (80° C) is reached, CO<sub>2</sub> is allowed to flow from the compressor through vessels A and B to the receiver and back to the compressor. When A is completely extracted, B is isolated, and the CO<sub>2</sub> from vessel A is allowed to equilibrate with vessel C. The CO<sub>2</sub> is then

FIGURE 2: SEMI-CONTINUOUS SUPERCRITICAL CO<sub>2</sub>-EXTRACTION SYSTEMS



pumped from vessel A to C until the pressure in A drops below supply pressure. Vessel A is then vented and the extracted soyflakes removed by vacuum. Carbon dioxide is then drawn from the supply cylinder and compressed to complete the filling of vessel C to 12,000 psi. The extraction now proceeds from B to C until B is extracted. At the same time, vessel A is refilled with soyflake, sealed and prepared for the third step (i.e., extraction from C to A), which completes one full cycle of this semicontinuous system.

**Quality of Oils Obtained by Supercritical CO<sub>2</sub> (SC-CO<sub>2</sub>) Extraction of Oilseeds at High Temperatures and Pressure**

Previous reports have described the quality of oils obtained by SC-CO<sub>2</sub> extraction of dry- and wet-milled corn germ,

soyflakes, and cottonseed flake at low temperatures and pressures (1 - 8). Table 2 presents the results of studies of these seed oils obtained (four liter Batch Autoclave) at optimum extraction temperatures (70-90° C) and pressure(12,000 psi). Included for comparison to the SC-CO<sub>2</sub> extracted oils are typical products obtained from reliable commercial sources. The crude-degummed soybean oil was obtained by solvent extraction with hexane while the dry-milled corn germ oil and cottonseed oil were recovered with expellers. SC-CO<sub>2</sub> extraction of soybean and dry-milled corn germ yields crude oils equivalent to or better than the commercially processed crudes with respect to color, fatty acid content, and refining loss.

Supercritical CO<sub>2</sub> extraction of cottonseed yields crude

**TABLE 2: SC-CO<sub>2</sub> EXTRACTION OF DRY-MILLED CORN GERM, SOY FLAKES AND COTTONSEED FLAKES AT HIGH TEMPERATURES AND PRESSURE**

CO <sub>2</sub> extraction temp. C	Pressure psi	Color <sup>a</sup>		FFA %	phos. ppm	Ref. loss %	Peroxide Value meq/kg
		Y	R				
<u>corn germ-oil</u>							
70	12,000	70	10	0.5	3	1.4	0
80	12,000	70	11	0.5	1	1.6	0
90	12,000	70	11	0.5	1	1.0	0
Comm'l expeller	—	70	12	0.7	120	1.6	0
<u>soy flakes-oil</u>							
70	12,000	70	12	0.3	1	0.5	0.1
80	12,000	70	12	0.3	1	0.6	0.2
90	12,000	70	12	0.3	1	0.5	0.2
Comm'l hexane degummed	—	70	10	0.3	90	1.0	0
<u>cottonseed flake-oil</u>							
70	12,000	70	16	1.2	2	1.4	0.1
80	12,000	70	20	1.2	5	1.5	0.2
90	12,000	70	20	1.2	13	1.5	0.1
Comm'l expeller	—	70	20	1.0	186	3.6	0

<sup>a</sup>Lovibond color scale, all values read at 5-1/4" depth except the crude commercial expeller cottonseed oil at 1" depth. 1600 g charge, 4 liter Batch Autoclave (4).



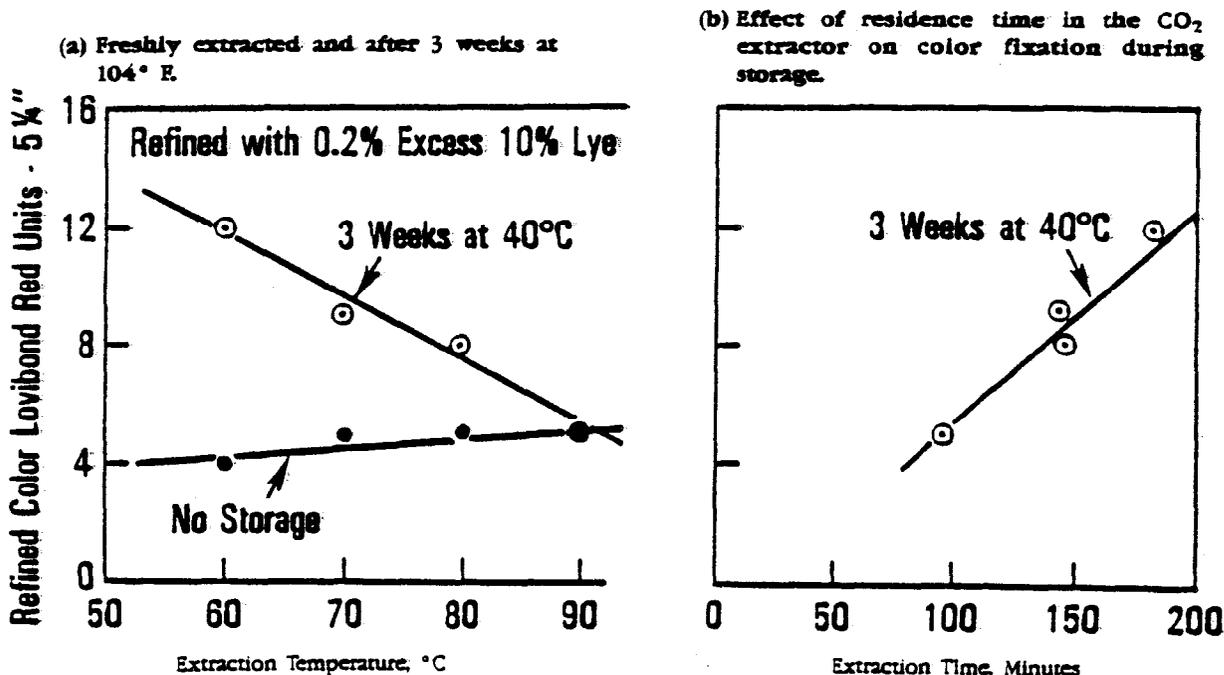
The processing of cottonseed oil obtained by SC-CO<sub>2</sub> extraction offers some potential saving over that obtained by expellers and solvent-extraction methods. Table 4 compares the savings realized in neutral oil yields and caustic soda costs for a plant refining 15 tank cars (60,000 lbs/car) of oil per day, 240 days a year. Assumptions are that the crude cottonseed oil contains 1.2 per cent free fatty acids and it is to be refined with ten per cent caustic soda  $\approx 14^\circ \text{Be}$  with 0.3 per cent excess for the expeller or solvent oil, and 0.1 per cent excess for the SC-CO<sub>2</sub>-extracted oil. The cost of the refining lye is calculated to be three cents/pound based on recent figures. The value of refined oil is assumed to be 20 cents/pound. At a two per cent increase in neutral oil from SC-CO<sub>2</sub> extraction, an additional 18,000 pounds of oil is obtained per day valued

at \$3,600, which over a 240-day operating schedule amounts to \$864,000.

Refining of crude expeller- or solvent-extracted cottonseed crude at 0.3 per cent excess caustic involves a cost of \$1,269/day for the lye, while an excess of 0.1 per cent costs the refiner \$729, or a savings of \$540/day. Similarly, over a 240-day operating year, a savings of \$130,000 would be realized. Thus, switching from solvent or expellers to CO<sub>2</sub>-extraction of cottonseed would yield a savings of nearly \$1,000,000/year by decreasing the lye requirements and increasing the yield of neutral oil.

The quality of corn oil, cottonseed oil, and soybean oil obtained at high extraction temperatures and pressure was investigated and results are shown in Table 5. Included for

FIGURE 3: COLOR FIXATION IN SUPERCRITICAL CO<sub>2</sub>-EXTRACTED COTTONSEED OIL



comparison are finished oils extracted at 50° C and 8,000 psi. Salad oils of good initial (0 time) quality will have a flavor of score 7.0-8.0 on a ten-point scale (ten = bland, one = extreme) and will score about six after four days' storage under Schall oven storage conditions (19). The results show that oils of good quality can be prepared from crude oils SC-CO<sub>2</sub> extracted at high temperatures. In addition, after four days' storage at 60° C, most of the flavor scores exceed six. SC-CO<sub>2</sub>-extracted soybean and corn oils, because of their low gum and free fatty acid contents, are ideal for steam refining; however, cottonseed oil is too dark for steam refining. Lovibond colors of both caustic- and steam-refined SC-CO<sub>2</sub> crude oils are much lighter than trading-rule specifications (20).

No evidence was found to indicate any increase in free fatty acids, color, refining losses, or impairment of flavor stability as a result of increasing SC-CO<sub>2</sub>-extraction parameters to 70-90° C and 12,000 psi.

#### Acknowledgements

J.H. Johnson assisted with the CO<sub>2</sub> extractions.

#### References

1. Friedrich, J.P., and G.R. List, *J. Agric. Food Chem.* 30:192 (1982).
2. Friedrich, J.P., G.R. List, and A.J. Heakin, *J. Am. Oil Chem. Soc.* 59:288 (1982).
3. Christianson, D.D., J.P. Friedrich, G.R. List, K. Warner, A.C. Stringfellow, E.B. Bagley, and G.E. Inglett, *J. Food Sci.* 49:229 (1984).
4. Friedrich, J.P., and E.H. Pryde, *J. Am. Oil Chem. Soc.* 61:5340 (1984).
5. List, G.R., J.P. Friedrich, and D.D. Christianson, *J. Am. Oil Chem. Soc.* 61:1847 (1984).
6. List, G.R., J.P. Friedrich, and J. Pominski, *Ibid* 61:1849 (1984).
7. List, G.R., and J.P. Friedrich, *Ibid* 62:82 (1985).
8. Friedrich, J.P., U.S. Patent 4,446,923, August 21, 1984.
9. Stahl, E., *Fette Siefen, Anstrichm* 84:444 (1982).
10. Stahl, E., E. Schultz, and W. Schütz, *J. Agri. Food Chem.* 28:1153 (1980).
11. Zhao, W., A. Shishikura, K. Jujimoto, K. Ari, and S. Saito, *Agric. Biol. Chem.* 51:1772 (1987).
12. Fattori, M., N.R. Bulley, and A. Meisen, *J. Agric. Food Chem.* 35:1739 (1987).
13. List, G.R., and J.P. Friedrich, *J. Am. Oil Chem. Soc.* 66:98-101 (1989).
14. Taniguchi, M., T. Tsuju, M. Shibuta, and T. Kobayashi, *Agric. Biol. Chem.* 49:2367 (1985).
15. Eissler, R., and J.P. Friedrich, *J. Am. Oil Chem. Soc.* 65:764-767 (1988).
16. Snyder, J.M., J.P. Friedrich, and D.D. Christianson, *Ibid* 61:1851 (1984).
17. Bailey, A.E., "Cottonseed and cottonseed products, their chemistry and technology," Interscience Publishers, New York (1984).
18. Vix, H.L.E., E.F. Pollard, J.J. Spadaro, and A. Gastrock, *Ind. Eng. Chem.* 38:635 (1946).
19. Evans, C.D., G.R. List, H.A. Moser, and J.C. Cowan, *JOACS* 50:218 (1973).
20. Federal Specifications, Salad Oil Vegetable III-S-309, Federal Supply Services, General Services Administration, March 24, 1978.

---

Presented at the 37th Oilseed Processing Clinic, held in New Orleans, Louisiana, March 14-15, 1988.

---

The mention of trade names or trade products does not imply that they are endorsed or recommended by the U.S. Department of Agriculture over other firms or similar products not mentioned.